

Probabilistic Damage Tolerance Fundamentals

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Nuss Sustainment Solutions



TEXTRON AVIATION



PDTA Basics

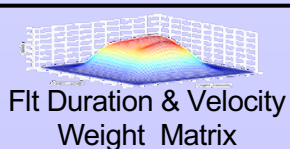
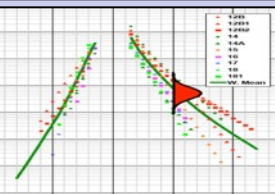
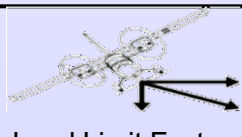
(Probabilistic Damage Tolerance Analysis)



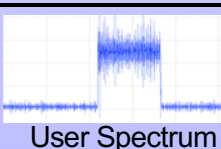
- PDTA considers variation in:
 - Initial flaw size
 - Material properties
 - Geometry
 - Usage and loads
 - Inspection reliability and probability of detection
 - Repair
- PDTA results in:
 - Single flight probability of failure at any time during operation

SMART | DTPDTA tool

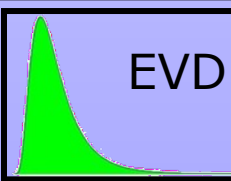
Loading Data



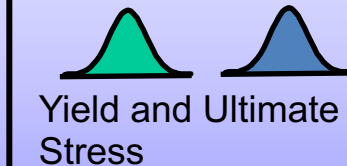
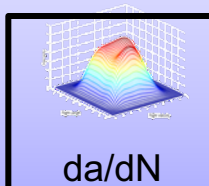
Internally Generated Loading



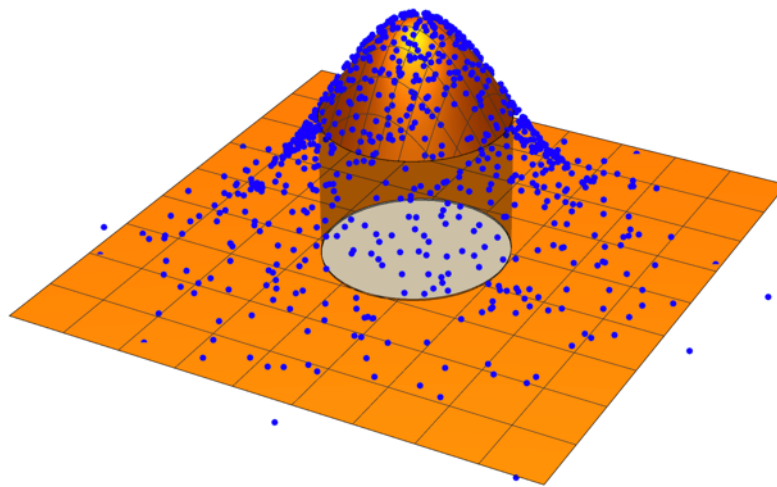
User Loading



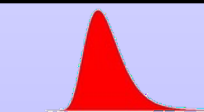
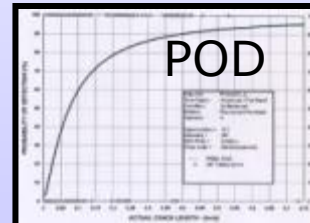
Material Data



Monte Carlo Sampling



Inspection Data

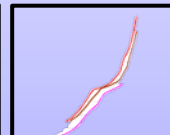
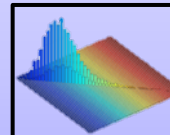
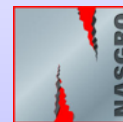


Repair Scenarios

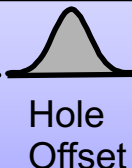
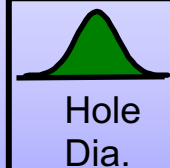
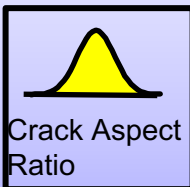
Inspection times

Prob. of Inspecting

Fracture Models



Geometry Data



Probability Equations



The probability-of-failure is the probability that maximum value of the applied stress (during the next flight) will exceed the residual strength σ_{RS} of the aircraft component

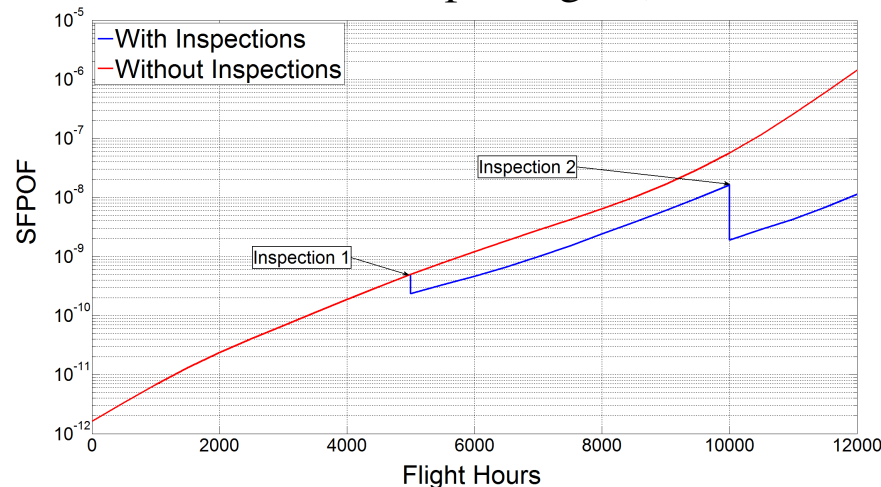
$$POF_{\text{no-surv}}(t) = P[\sigma_{Max} > \sigma_{RS}(t)] = \int [1 - F_{EVD}(\sigma_{RS}(t))] f_{\mathbf{x}}(\mathbf{x}) d\mathbf{x}$$

$$CTPOF(t) = \int \left[1 - \prod_{i=1}^t F_{EVD}(\sigma_{RS}(t_i)) \right] f_{\mathbf{x}}(\mathbf{x}) d\mathbf{x}$$

$$POF_{\text{surv}}(t) = \int \left[\prod_{i=1}^{t-1} F_{EVD}(\sigma_{RS}(t_i)) \right] [1 - F_{EVD}(\sigma_{RS}(t))] f_{\mathbf{x}}(\mathbf{x}) d\mathbf{x}$$

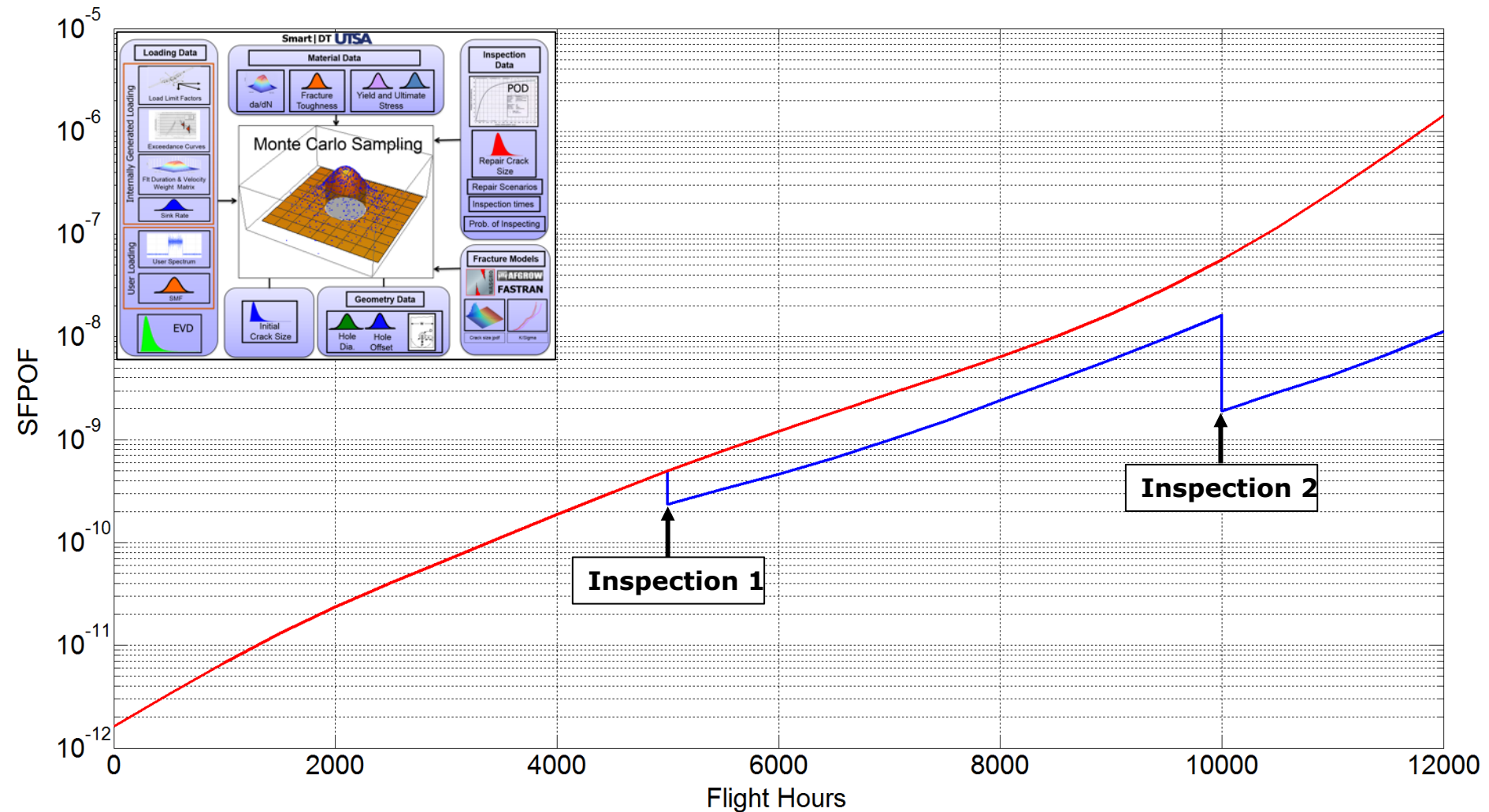
$$Hz(t) = \frac{POF_{\text{surv}}(t)}{1 - CTPOF(t)}$$

F_{EVD} = CDF of maximum stress per flight (extreme value distribution).



PDTA Results: SFPOF

(SFPOF: Single Flight Probability Of Failure)



Random Variable Summary



Random Variable	SMART DT Options
Initial Crack Size	Lognormal, Weibull, Tabular, Tabular joint a and c
Fracture Toughness	Normal, Tabular
Extreme Load per Flight	Gumbel, Weibull, Frechet
da/dN Parameters	Correlated normal
Crack Aspect Ratio	Normal, Tabular
Hole Diameter	Normal, Tabular
Hole Offset	Normal
Yield Stress	Normal
Ultimate Stress	Normal
Peak Stress	Uniform

Expandable

SMART|DT Loading Exceedance Options



Usages
Single-Engine Unpressurized Usage Basic Flight Instruction
Single-Engine Unpressurized Usage Personal Usage
Single-Engine Unpressurized Usage Executive Usage
Single-Engine Unpressurized Usage Aerobatic Usage
Twin-Engine Unpressurized Usage Basic Flight Instruction
Twin-Engine Unpressurized Usage General
Pressurized Usage
Agricultural/Special Usage
User defined

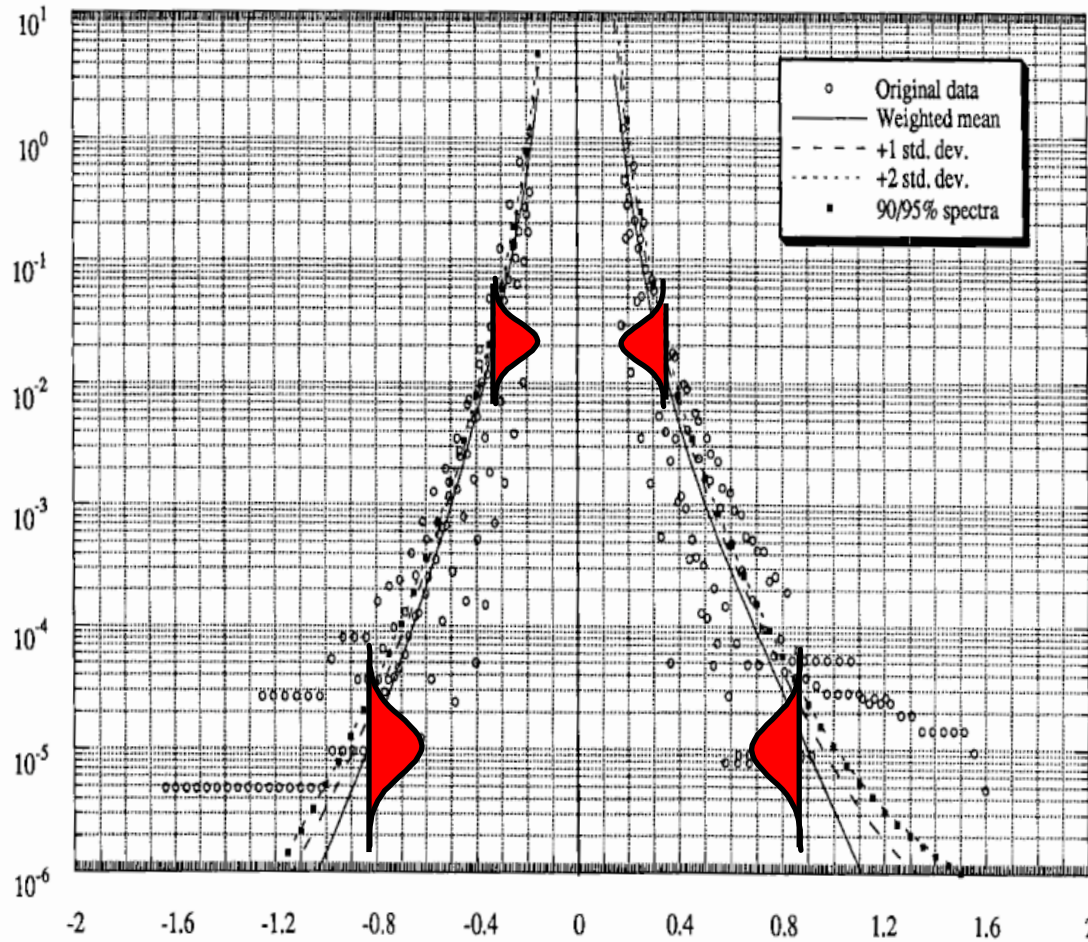
Note: exceedance data are normalized to velocity and limit load factor

Mix of weighted usages allowed

Loading Generation

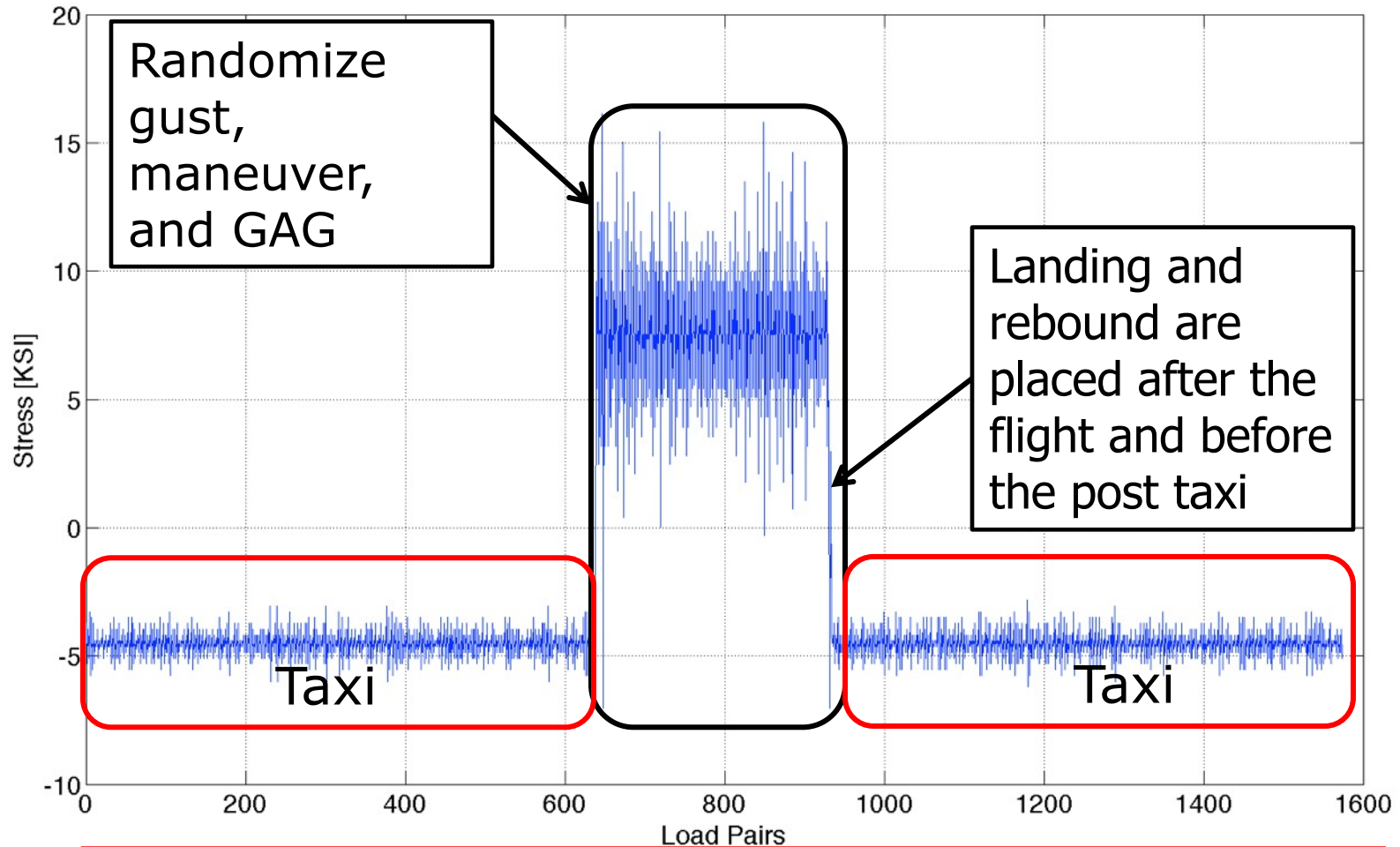


Exceedances/
Nautical Mile



Acceleration Fraction, a_n/a_{nLLF}

Loading Example



Randomize taxi loads and split half before the flight and half after the flight. Taxi load can be excluded from the analysis.

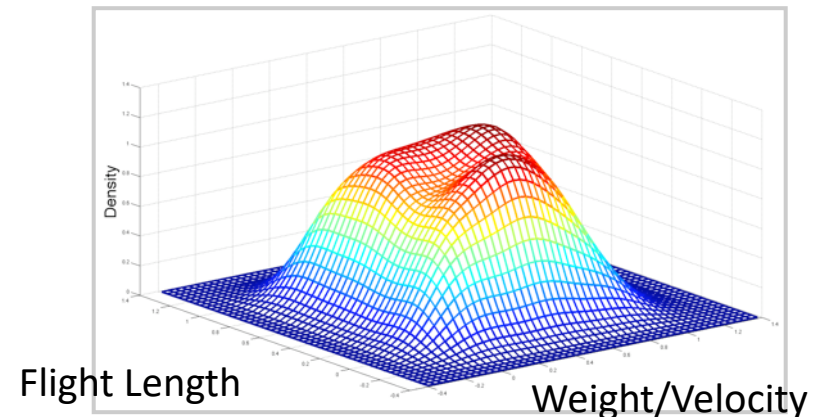
Usage and Loads



- SMART uses two matrices to account for variation in:
 - Flight length
 - Flight velocity
 - Flight weight
- Matrices can describe fleet variation, or
- Matrices can describe flight profiles

Flight Length and Weight/Velocity Matrix

Flight time (Hours)	% of Flights	Weight (1g_stress and Ground_stress) Percentage						
		1.00	0.95	0.90	0.85	0.80	0.75	0.70
0.25	0.00	0	0	0	0	0	0	0
0.50	0.05	0	0	0.05	0.25	0.6	0.1	0
0.75	0.15	0	0	0.25	0.4	0.3	0.05	0
1.00	0.35	0.05	0.15	0.45	0.3	0.05	0	0
1.25	0.10	0.05	0.15	0.45	0.3	0.05	0	0
1.50	0.10	0.05	0.3	0.5	0.15	0	0	0
1.75	0.20	0.05	0.3	0.5	0.15	0	0	0
2.00	0.05	0.15	0.55	0.2	0.1	0	0	0



Usage Variation - Fleet



Mission	Mission Name	% of flights	Flight Duration (hr)	MTOW (lb)	Cruise Speed (Kts)
A	Check ride	10%	0.2	5200	160
B	High speed cruise	20%	0.9	6800	180
C	Max weight	30%	1.1	7000	175
D	Max range	40%	3	6600	170

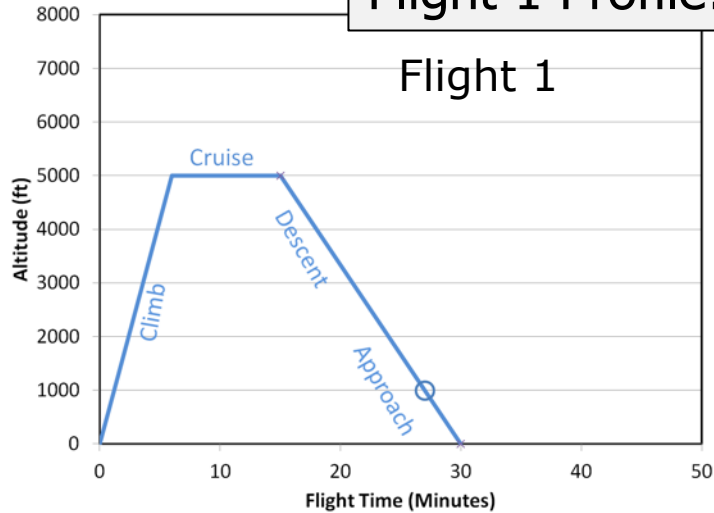
Mission	Flight time (Hours)	% of Flights (sums to 1.0)	Average Speed During Flight, % Design Velocity			
			0.8	0.9	0.0875	0.85
			% of Flights (sums to 1.0)			
A	0.2	0.1	1.0	0	0	0
B	0.9	0.2	0	1.0	0	0
C	1.1	0.3	0	0	1.0	0
D	3.0	0.4	0	0	0	1.0

Mission	Flight time (Hours)	% of Flights (sums to 1.0)	Average Weight During Flight, % Design Weight			
			0.74	0.97	1.00	0.94
			% of Flights (sums to 1.0)			
A	0.2	0.1	1.0	0	0	0
B	0.9	0.2	0	1.0	0	0
C	1.1	0.3	0	0	1.0	0
D	3.0	0.4	0	0	0	1.0

Usage Variation – Flight Profiles



Flight 1 Profile: TE unpress. general usage

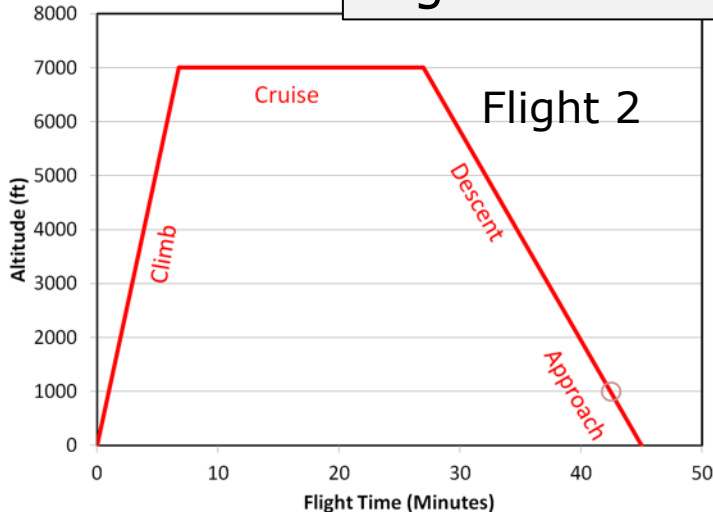


Segment	Weight	KEAS	% Duration
CLIMB	6580	140	0.20
CRUISE	6440	160	0.50
DESCENT	6300	180	0.20
APPROACH	6160	120	0.10

$$V_C = 200 \text{ KEAS}$$

$$\text{MTOW} = 7000 \text{ lb}$$

Flight 2 Profile: TE unpress. general usage



Segment	Weight	KEAS	% Duration
CLIMB	6720	140	0.15
CRUISE	6580	160	0.60
DESCENT	6440	180	0.15
APPROACH	6300	120	0.10

$$V_C = 200 \text{ KEAS}$$

$$\text{MTOW} = 7000 \text{ lb}$$

Usage Variation – Flight Profiles



Flight 1 Profile:
TE unpress. general usage

Flight time (Hours)	% of Flights (sums to 1.0)	Average Speed During Flight, % Design Velocity				
		0.6	0.7	0.8	0.9	1.0
		% of Flights (sums to 1.0)				
0.5	1	0.1	0.2	0.5	0.2	0

Flight time (Hours)	% of Flights (sums to 1.0)	Average Weight During Flight, % Design Weight				
		0.88	0.9	0.92	0.94	0.96
		% of Flights (sums to 1.0)				
0.5	1	0.1	0.2	0.5	0.2	0

Flight 2 Profile:
TE unpress. general usage

Flight time (Hours)	% of Flights (sums to 1.0)	Average Speed During Flight, % Design Velocity				
		0.6	0.7	0.8	0.9	1.0
		% of Flights (sums to 1.0)				
0.75	1	0.1	0.15	0.6	0.15	0

Flight time (Hours)	% of Flights (sums to 1.0)	Average Weight During Flight, % Design Weight				
		0.88	0.9	0.92	0.94	0.96
		% of Flights (sums to 1.0)				
0.75	1	0	0.1	0.15	0.6	0.15

EVD Generation

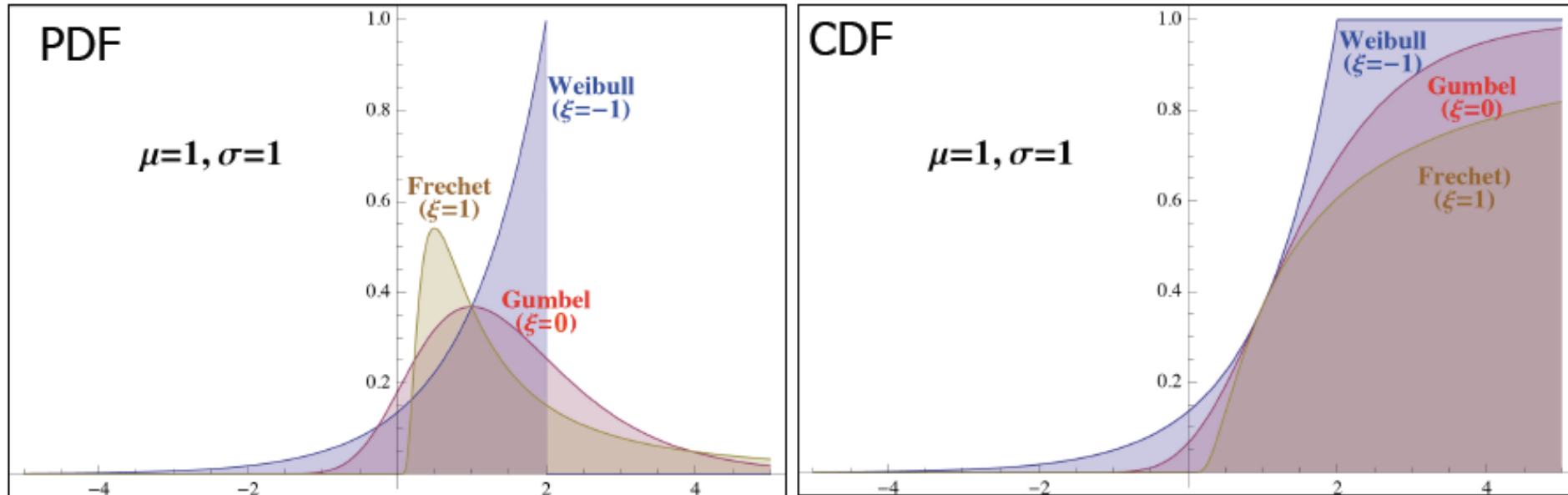
(Extreme Value Distribution)



- Maximum Weibull, Frechet, or Gumbel can be written in terms of the Generalized Extreme Value Distribution as

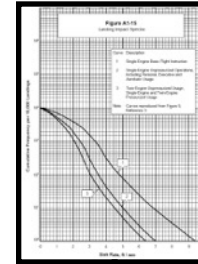
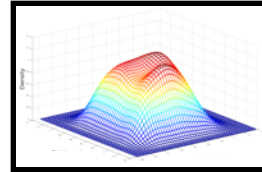
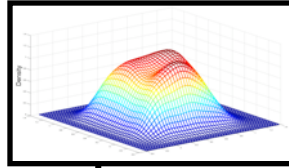
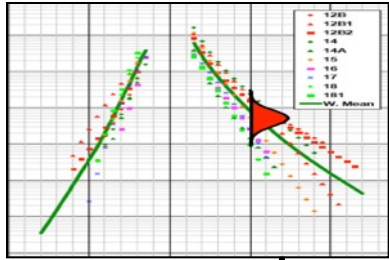
$$F(x) = \exp \left\{ - \left[1 + \xi \left(\frac{x - \mu}{\sigma} \right) \right]^{-1/\xi} \right\} \begin{array}{ll} \xi = 0 & \text{Gumbel} \\ \xi > 0 & \text{Frechet} \\ \xi < 0 & \text{Weibull} \end{array}$$

- Parameters (μ, σ, ξ) location, scale, and shape define the distribution.

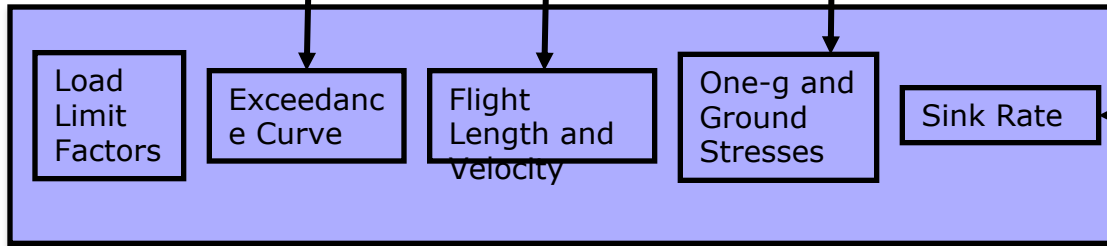


Maximum likelihood estimation

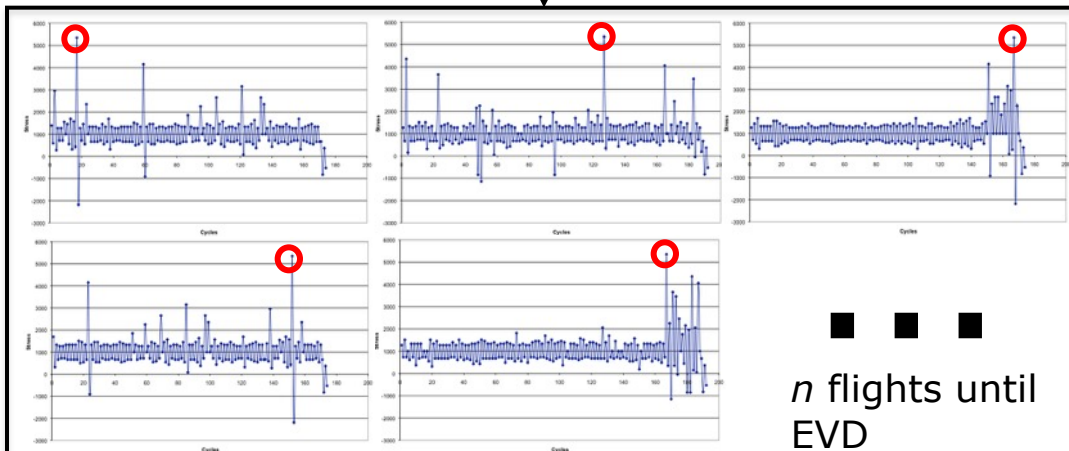
EVD Generation (Extreme Value Distribution)



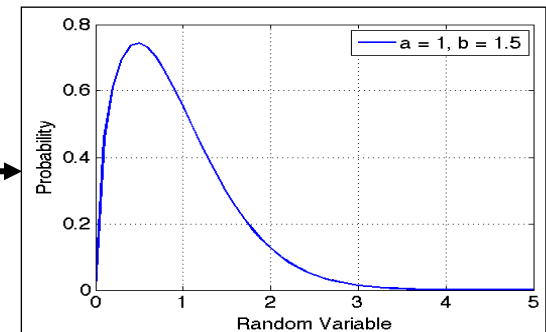
✓ EVD computed internally from spectrum



$$F(x) = \exp \left\{ - \left[1 + \xi \left(\frac{x - \mu}{\sigma} \right) \right]^{-1/\xi} \right\}$$



EVD Distribution



Residual Strength Interpolation

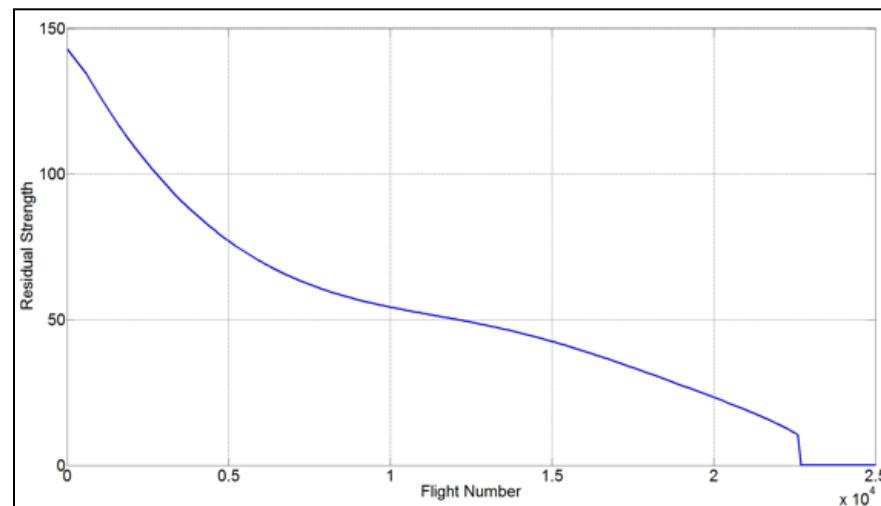


- From Fracture Mechanics we know:

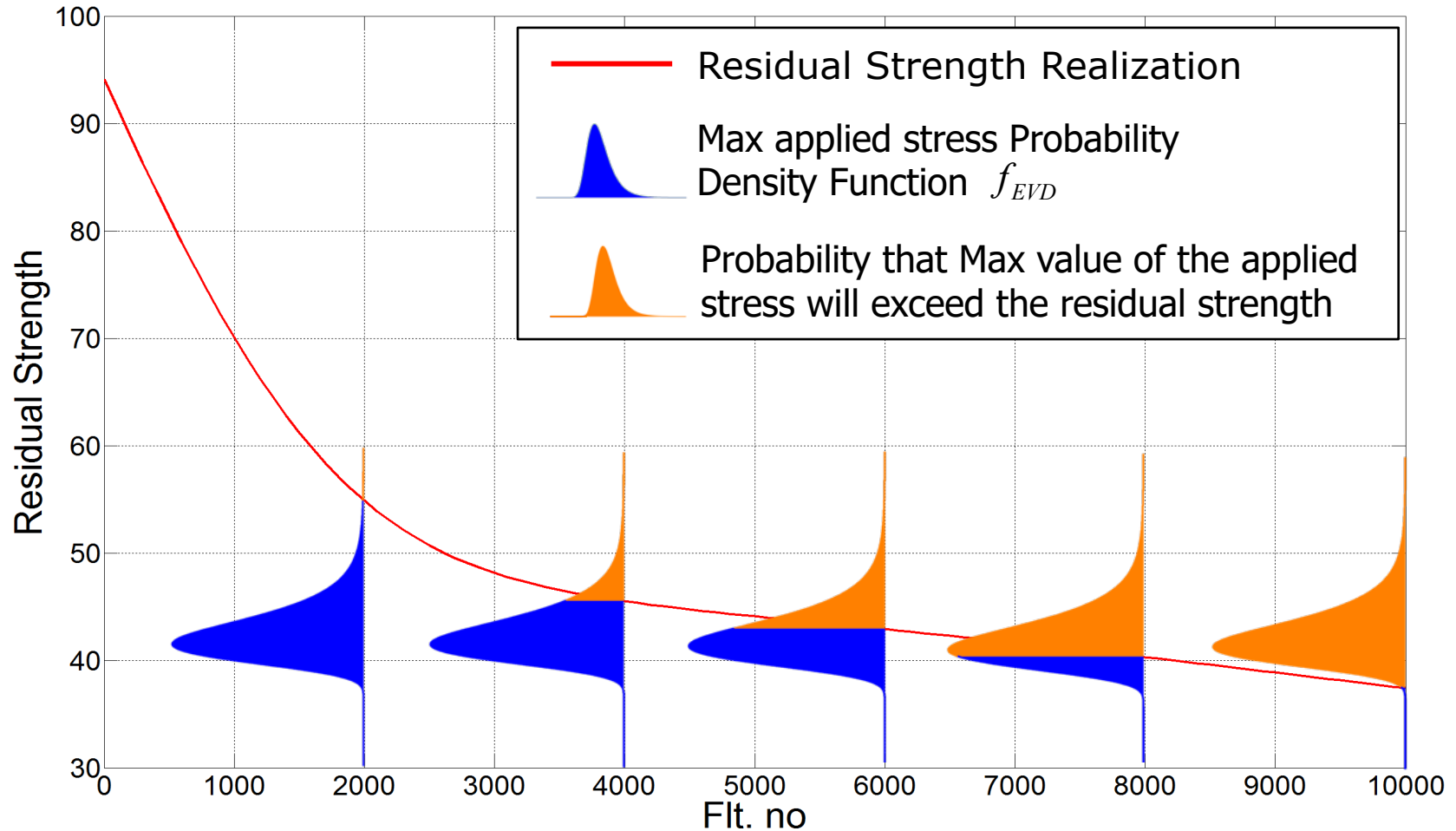
$$K_C = \sigma_{RS} \beta(a(a_o, t)) \sqrt{\pi a(a_o, t)}$$

- Residual Strength can be defined as:

$$\sigma_{RS} = \frac{K_C}{\beta(a(a_o, t)) \sqrt{\pi a(a_o, t)}}$$



Probability of Failure



$$POF(t|a_i K_C) = 1 - F_{EVD} \left(\frac{K_C}{\beta(a(a_o, t)) \sqrt{\pi a(a_o, t)}} \right)$$

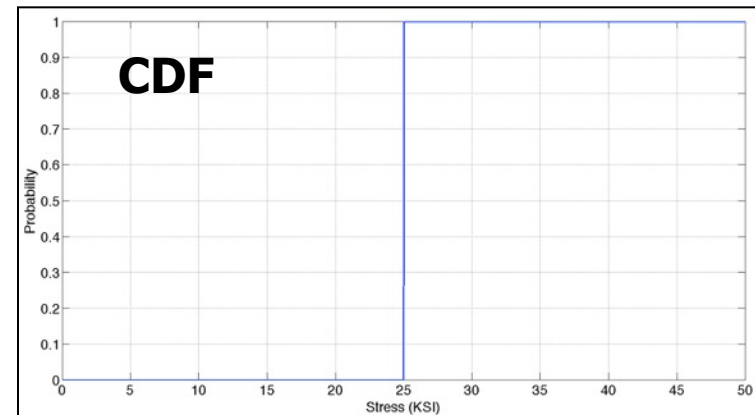
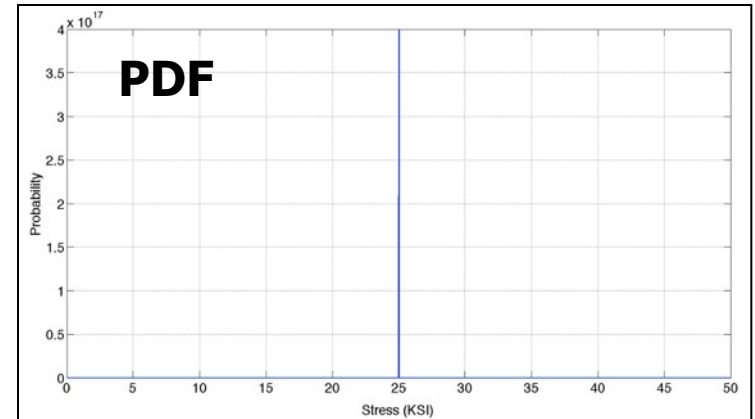
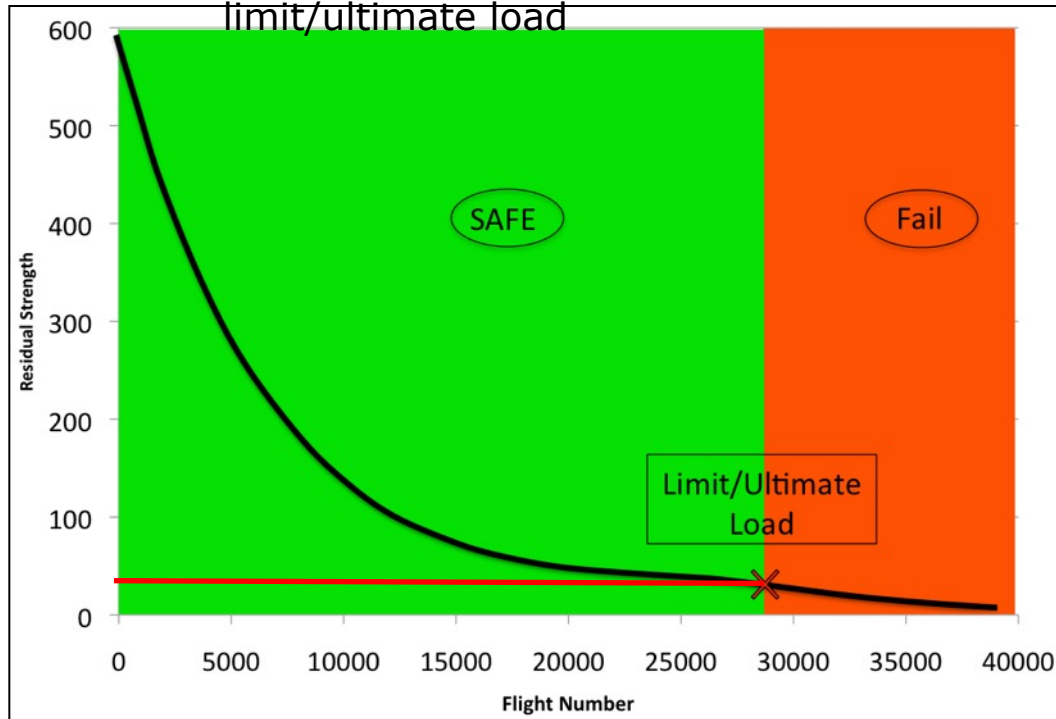
Limit/Ultimate Load EVD



Smart|DT allows the user to input the limit load as a deterministic EVD input.

- Residual strength \leq limit load has a POF = 1
- Residual strength $>$ limit load has a POF = 0

EVD is set to a deterministic value equal to the airplane limit/ultimate load



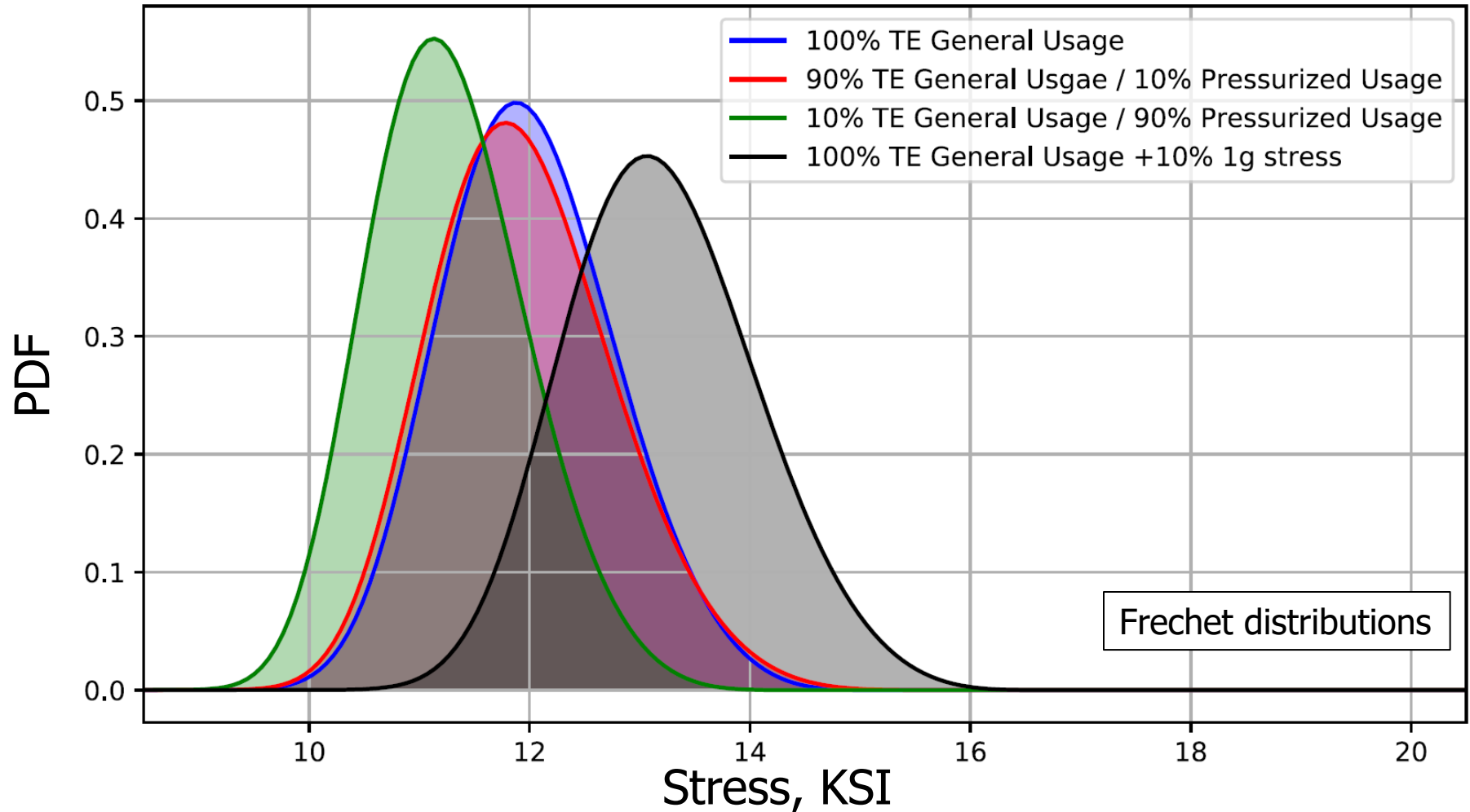
Comparison of EVD



Usage	EVD Parameters		
	Location μ	Scale σ	Shape ξ
100% TE General Usage	11.697	0.757	0.218
90% TE General Usage/10% Pressurized usage	11.625	0.779	0.187
10% TE General Usage/90% Pressurized usage	10.984	0.680	0.197
(All 1g stress = 5700 psi)			
100% TE General Usage +10% 1g stress	12.866	0.833	0.218

EVD: Extreme Value Distribution

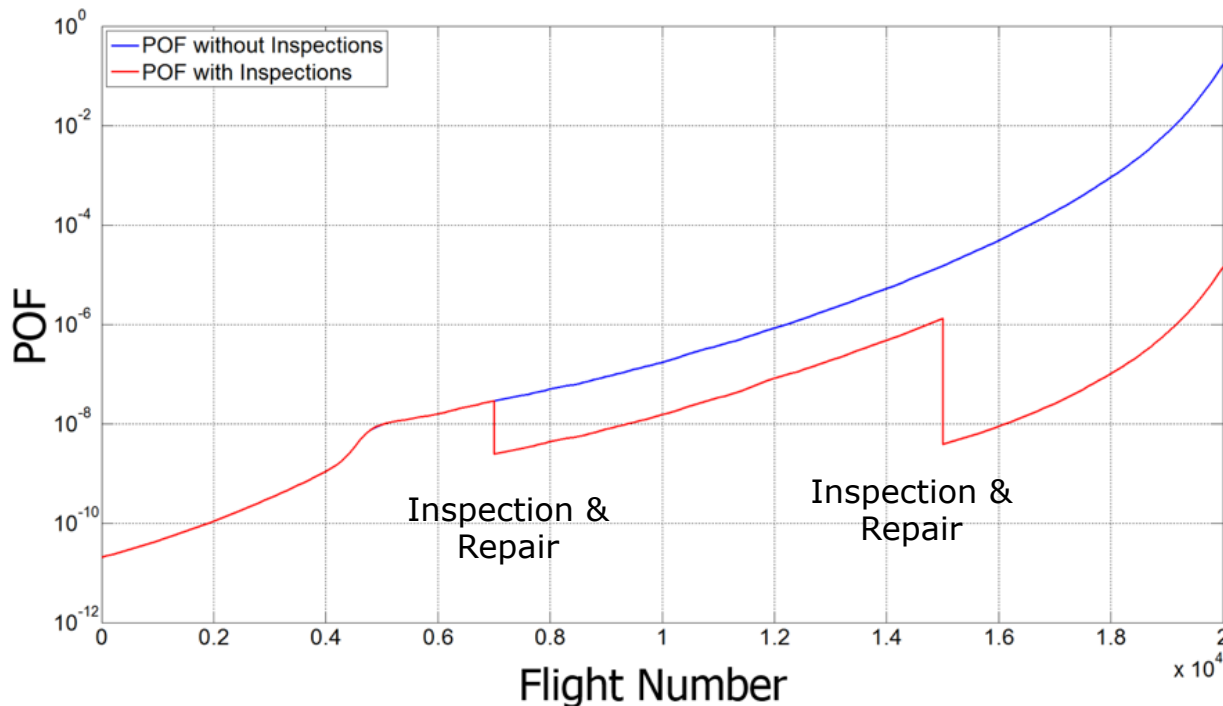
Comparison of EVD



Inspections



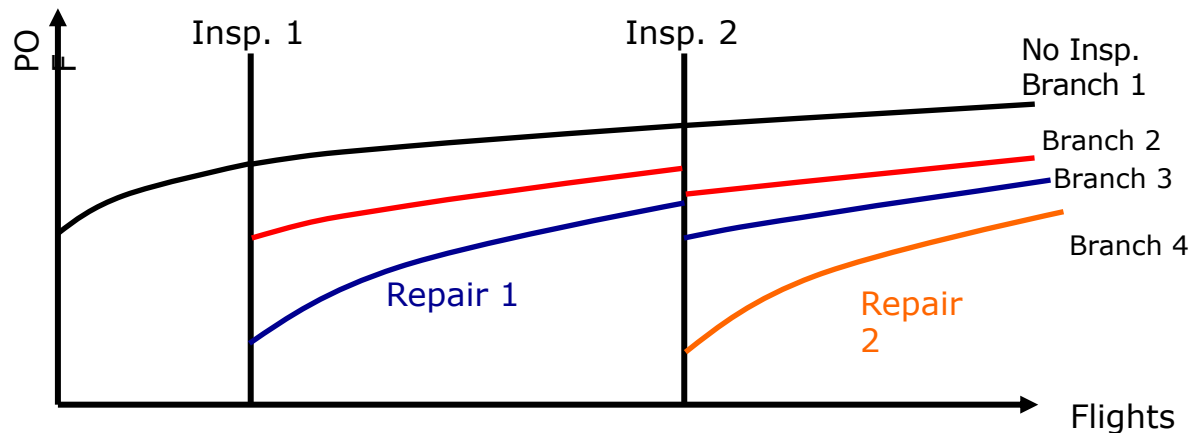
- ❑ Probability of Detection (POD)
- ❑ Probability of Inspection (POI)
- ❑ Inspection times
- ❑ After inspection and/or repair crack size





- Treat inspections as multiple “branches” where each branch represents a repair scenario.
- Each branch computed independently.
- Overall POF determined as a sum from all branches.

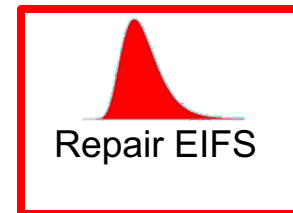
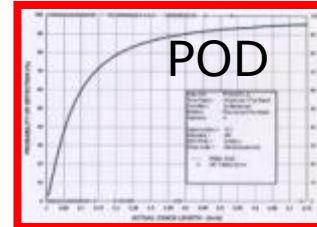
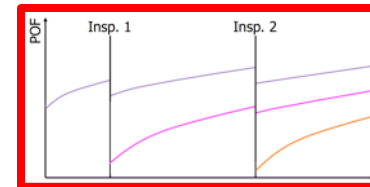
POD, POI and “after repair initial crack size” can be changed for each branch (different repair scenarios can be analyzed).



Inspection Capabilities



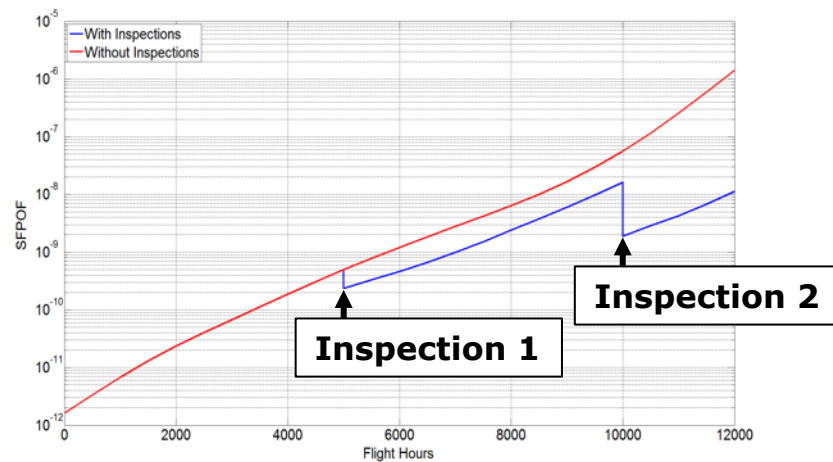
- Smart|DT has robust inspection and repair capabilities:
 - Any number of inspections at user-defined flights
 - Different scenarios for each inspection
 - POD curve inputs (deterministic, tabular, lognormal)
 - Probability of Inspection
 - Arbitrary repair EIFS (deterministic, tabular, lognormal, Weibull)



Summary



- PDTA quantifies risk by considering variation in initial flaw size, material, geometry, usage, inspection, etc.
- PDTA tools are useful to assess usage severity variation
 - Especially important when assessing in-service issues
- PDTA tools incorporate effects of inspections and repair to assess risk for various repair scenarios





Monte Carlo Sampling

Outline

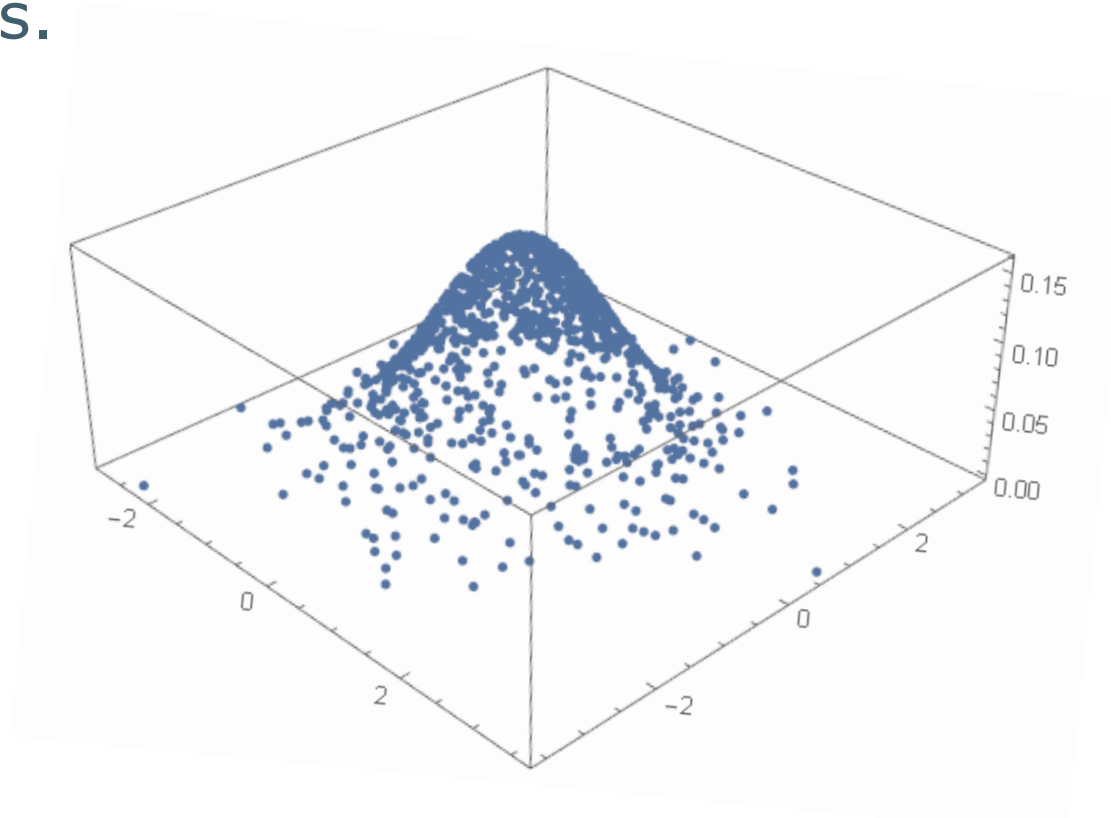


- ✓ Basics of Monte Carlo sampling
 - ✓ Limit state
 - ✓ Indicator function
 - ✓ Academic Excel example
 - ✓ How to generate samples to compute pi (3.1416)
- ✓ PDTA Example (Generate samples for Kc and MaxLoad)
 - ✓ Define limit state
 - ✓ Setting confidence limits as a function of the number of samples

Monte Carlo Sampling



Monte Carlo sampling is a technique to evaluate difficult integrals (multi-dimensional) or to sample random variables governed by probability density functions.



The Limit State

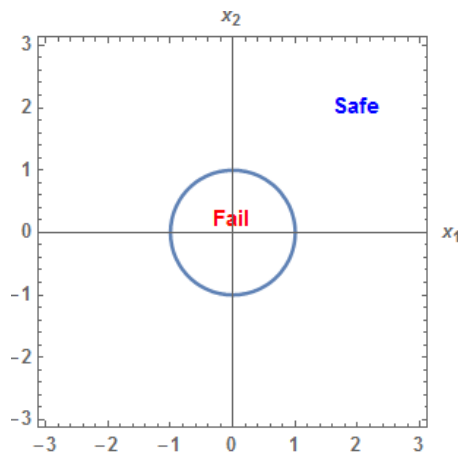


The limit state “g” is used to define the failure domain.
The definition of failure is always rewritten such that:

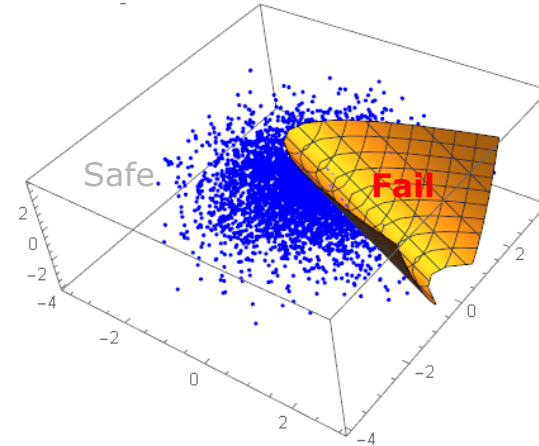
$g(x) = 0$ - limit state

$g(x) \leq 0$ - failure

$g(x) > 0$ - safe



$$x_1^2 + x_2^2 - 1 = 0$$



$$\frac{x_3}{2} - x_2^2 + x_1 - 1 = 0$$

Typical engineering examples of limit states



- ✓ yield stress $<$ stress
- ✓ clearance $<$ max allowable displacement
- ✓ fracture toughness $<$ stress intensity factor
- ✓ critical crack size $<$ growing crack size
- ✓ material thickness $<$ corrosion depth
- ✓ vibration amplitude $<$ max. allowable amp.

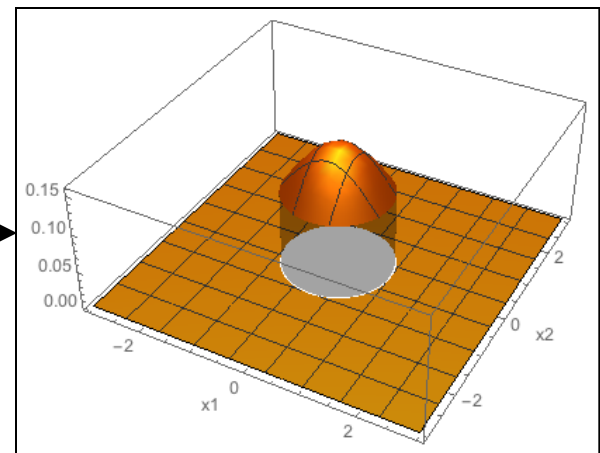
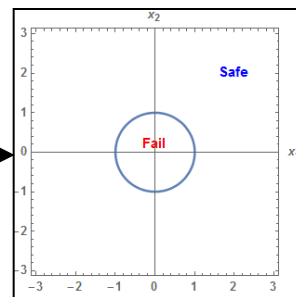
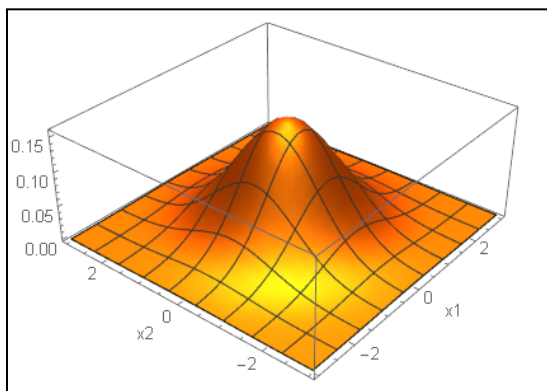
Indicator Function



To compute the probability of failure, the binary indicator function is used:

$$P_f = \int_{-\infty}^{\infty} I(\mathbf{x}) f_{\mathbf{x}}(\mathbf{x}) d\mathbf{x}$$

The indicator function is a binary, 1 or 0, function defined as equal to "1" in the failure domain and "0" in the safe domain



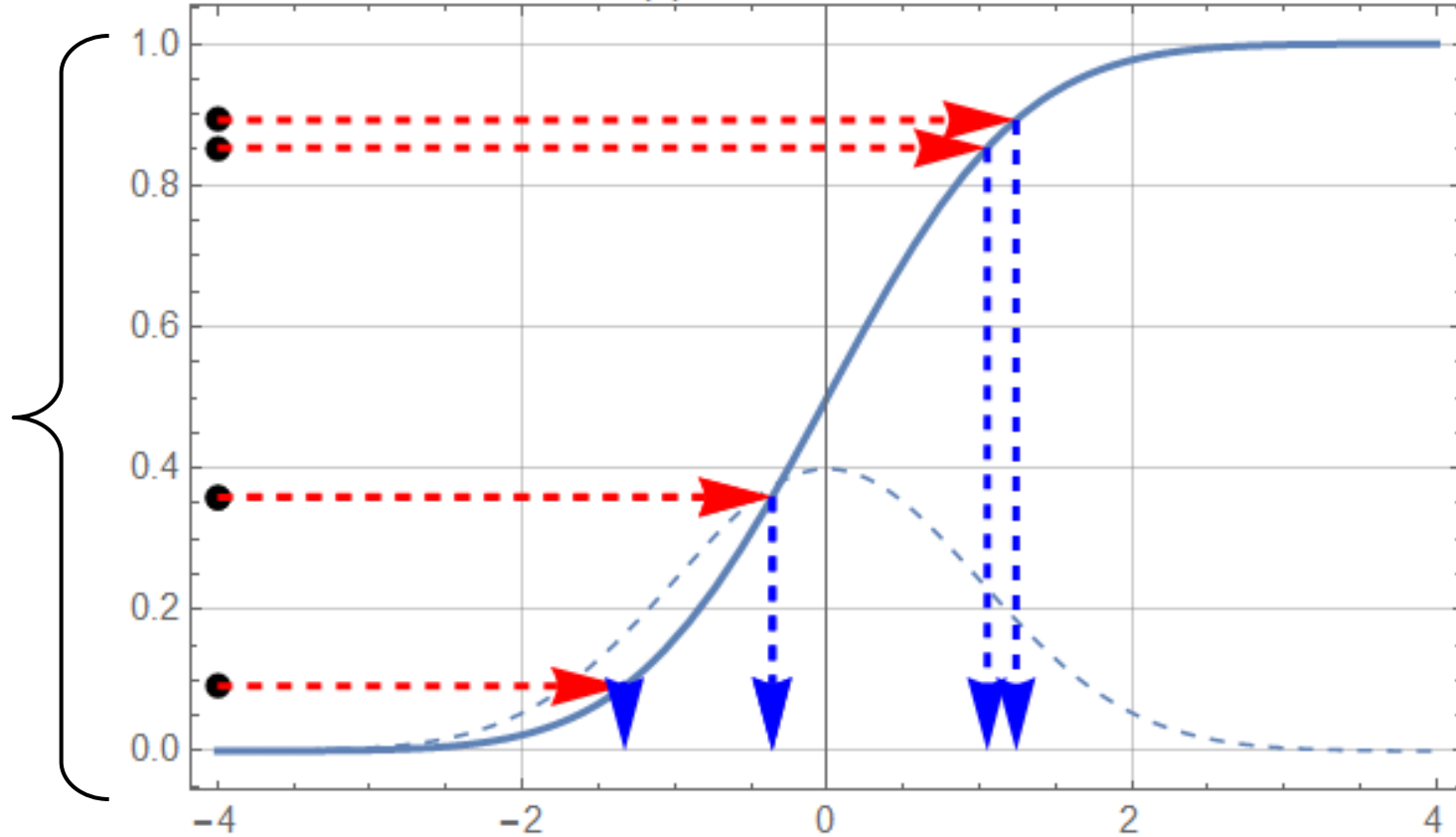
How to Generate Samples



Random Sampling (Inverse Integral Method)

$\Phi(x)$ - Standard Normal

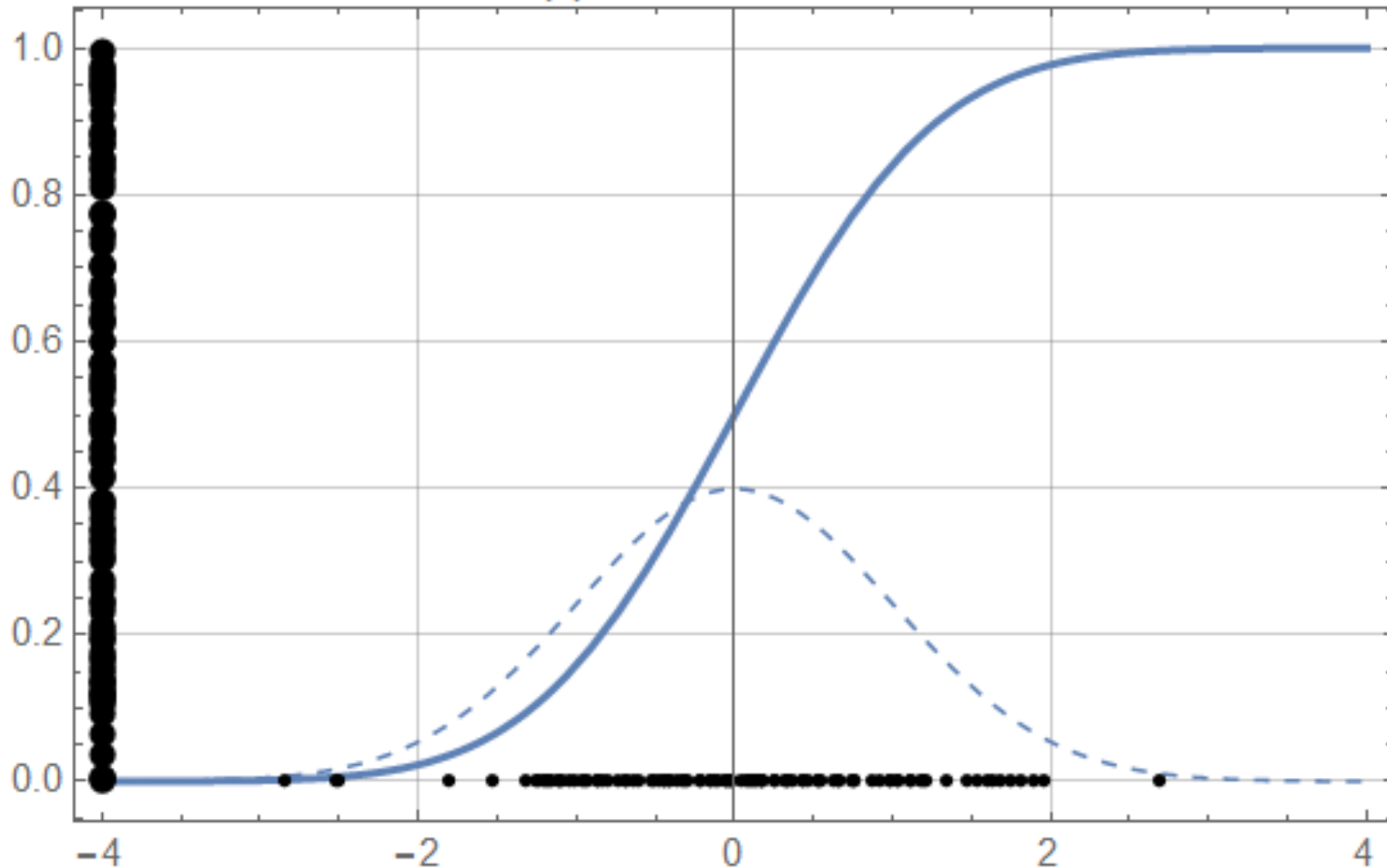
Uniformly distributed random numbers



How to Generate Samples



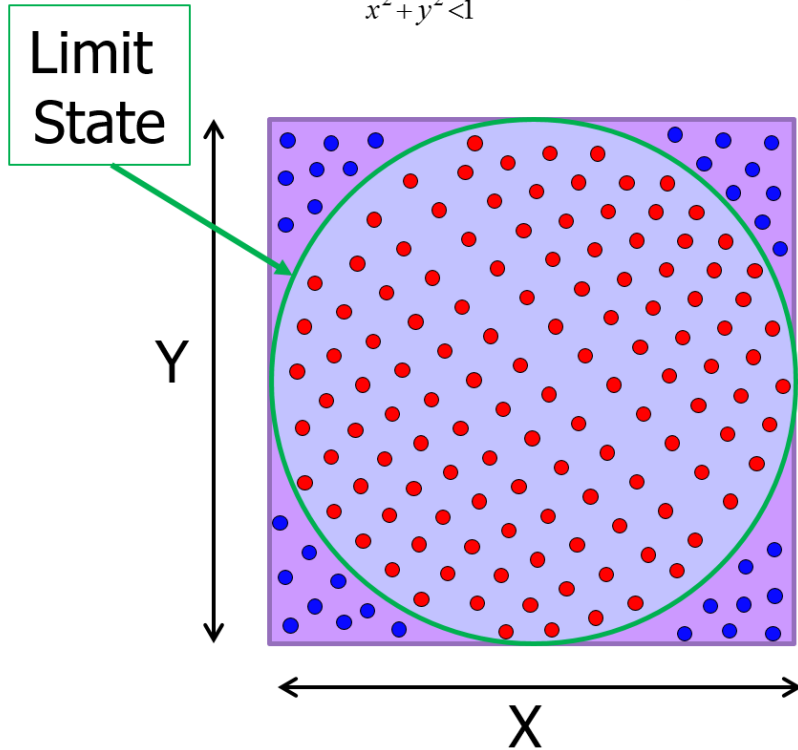
$\Phi(x)$ - Standard Normal



A simple Monte Carlo Example



$$A = \int_{x^2+y^2 < 1} \int dx dy = \frac{\pi}{4}$$

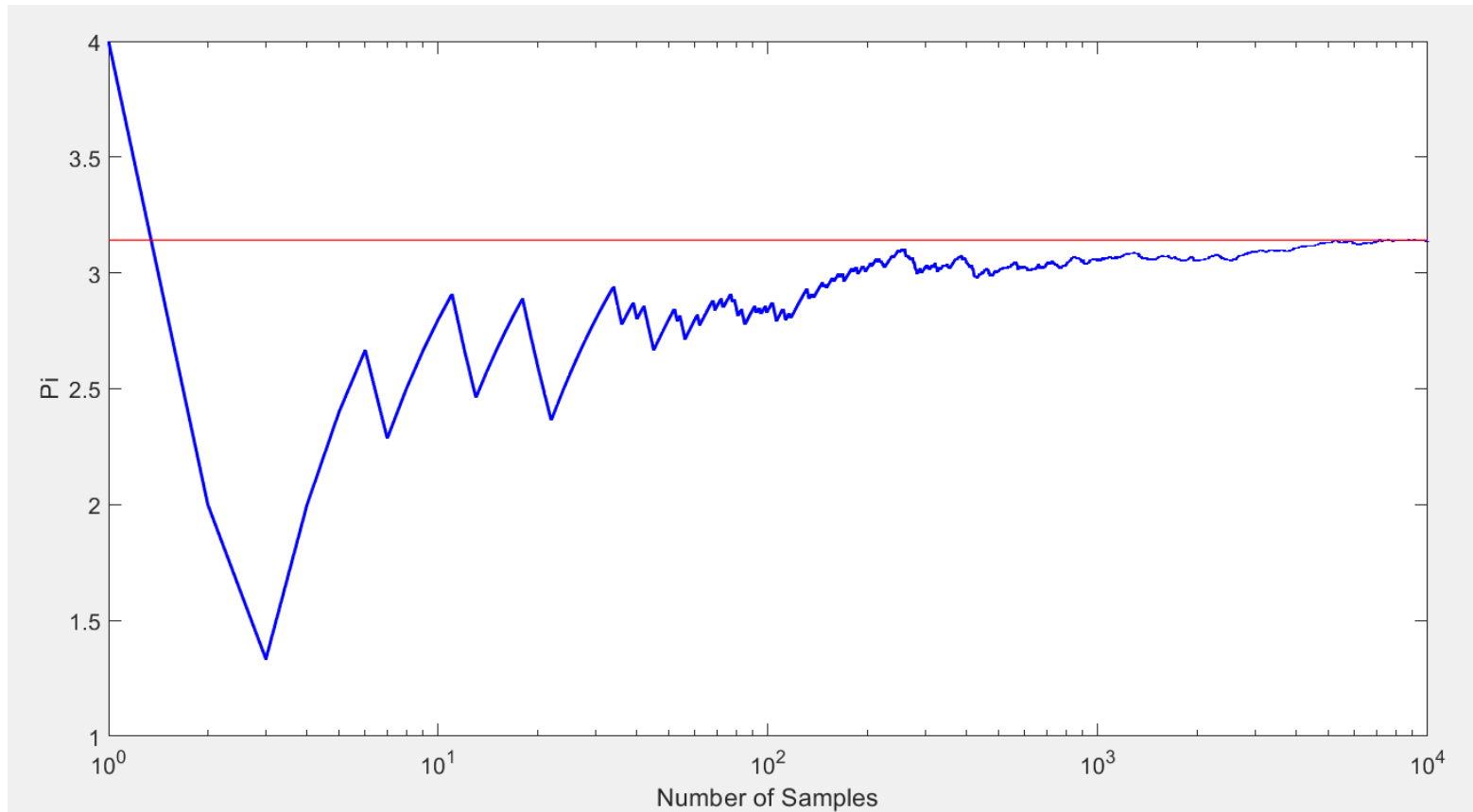


$$x_1^2 + x_2^2 - 1 \leq 0$$

- How Monte Carlo Works:
1. Randomly select a large number of points inside the square (Domain).
 2. Count how many points lands inside the circle
 3. Divide by the total number of points on the domain
 4. The answer is exact when the number of points goes to infinite

Excel exercise

Convergence wrt Number of Samples



Excel exercise

PDTA Example

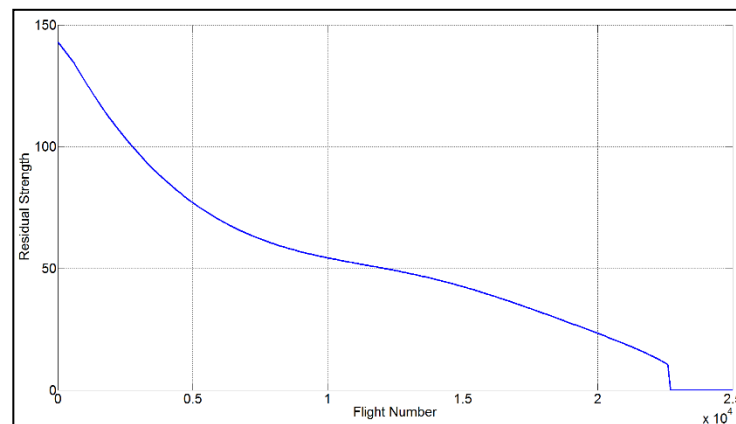


The Residual Strength (RS) at a given time is:

$$\sigma_{RS}(t) = \frac{K_C}{\beta(a(a_o, t))\sqrt{\pi a(a_o, t)}}$$

Having the maximum load per flight, the limit state is:

$$g(x) \Rightarrow \sigma_{RS}(t) - MaxLoad < 0$$



PDTA Example



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Excel exercise

PDTA Example



Steps:

1. Generate MaxLoad realizations $G \sim (0.8, 0.5)$
2. Generate Fracture Toughness (K_c) realizations $N \sim (34.5, 3.8)$
3. Generate Residual Strength as:

$$\sigma_{RS}(t) = \frac{K_{c_i}}{\alpha(8000 FH)} = \frac{K_{c_i}}{2.8}$$

4. Evaluate the limit state using the indicator function

$$\text{If } \sigma_{RS}(t) > \text{MaxLoad} \rightarrow I(x) = 0$$

$$\text{If } \sigma_{RS}(t) < \text{MaxLoad} \rightarrow I(x) = 1$$

5. Count the number of failures ($\text{Sum}(I(x))$) and compute the POF as

$$POF(t) = \frac{\text{sum}(I(x))}{\# \text{ Sampoes}}$$

POF Convergence wrt Number of Samples



- The standard deviation of the probability estimate reduces as the square root of the number of samples.

$$\sigma_{\bar{P}} = \sqrt{\frac{\bar{P}(1 - \bar{P})}{N}}$$

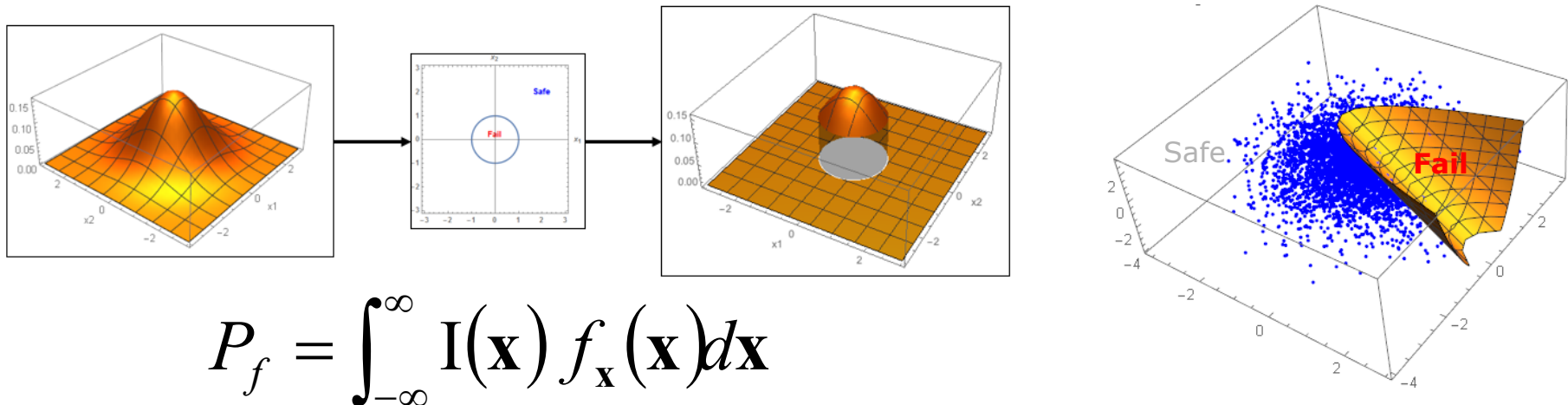
$$\delta_{\bar{P}} = \sqrt{\frac{(1 - \bar{P})}{\bar{P}N}}$$

$$N = \frac{1 - \bar{P}}{\bar{P}\delta_{\bar{P}}}$$

Summary



- Basics of Monte Carlo sampling were reviewed
 - Limit state and Indicator function
- PDTA Example (Generate samples for Kc)
 - Define limit state
 - Setting confidence limits as a function of the number of samples



Questions

